

# International Journal of Innovative Research in Science, Engineering and Technology

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# Design and Analysis of Die and Punch on Thinning Sheet in Deep Drawing Process

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**ABSTRACT:** Deep drawing is a sheet metal forming process in which a sheet metal blank is radially drawn into a forming die by the mechanical action of a punch. The process is considered "deep" drawing when the depth of the drawn part exceeds its diameter. The model is designed in CREO software. Analysis is done in ANSYS software for different materials in this work the stress have been calculated theoretically as well as Ansys and both results are compared. Modal analysis is done for cup to determine the deformation and frequency for different materials by changing the geometry thicknesses. Random vibration analysis is done for die to determine the directional deformation, shear stress and shear strain for different materials by changing the geometry thickness. Transient analysis is done for die to determine the deformation, stress and strain for different materials by changing the geometry thickness with respect to time. From the static analysis of die and punch AL5083 material having minimum stress value compared to AL7475 and stainless steel. So it can be concluded the geometry thickness is 0.9 mm and material is AL 5083 is best for die and punch.

#### I. INTRODUCTION

Deep drawing is a sheet metal forming process in which a sheet metal blank is radially drawn into a forming die by the mechanical action of a punch. It is thus a shape transformation process with material retention. The process is considered "deep" drawing when the depth of the drawn part exceeds its diameter. This is achieved by redrawing the part through a series of dies. The flange region (sheet metal in the die shoulder area) experiences a radial drawing stress and a tangential compressive stress due to the material retention property. These compressive stresses (hoop stresses) result in flange wrinkles (wrinkles of the first order). Wrinkles can be prevented by using a blank holder, the function of which is to facilitate controlled material flow into the die radius

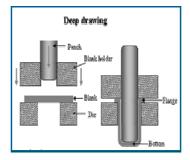


FIG1: A Typical Deep Drawing Operation

The total drawing load consists of the ideal forming load and an additional component to compensate for friction in the contacting areas of the flange region and bending forces as well as unbending forces at the die radius. The forming load is transferred from the punch radius through the drawn part wall into the deformation region (sheet metal flange).



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In the drawn part wall, which is in contact with the punch, the hoop strain is zero whereby the plane strain condition is reached. In reality, mostly the strain condition is only approximately plane. Due to tensile forces acting in the part wall, wall thinning is prominent and results in an uneven part wall thickness, such that the part wall thickness is lowest at the point where the part wall loses contact with the punch, i.e., at the punch radius.

#### II. LITERATURE REVIEW

Jay N.Mistri, K.D.Kothari, Gaurav, Kumar Sharma all[1], are discussed about Deep drawing is part of forming process in which sheet metal drawn into die cavity by action of a punch. So, due to action of punch desired shape can be achieved. For reduce various defects in deep drawing process it is essential to control or vary physical and geometric parameters of deep drawing process. Sheet-metal drawing is a more complex operation than cutting or bending, and more things can go wrong. Nowadays composite material is extensively used in manufacturing industries due to its better strength.

KrupalT.Shah,SandipChaudhary,DarshanK.Bhatt[2], are discussed about Deep drawing process is a sheet metal forming process where a punch is utilized to force a flat sheet metal to flow into the gap between the punch and die surfaces. As a result, the sheet metal or blank will deformed into desired shape like cylindrical, conic, or boxed shaped part and also complex parts.

Chandra Pal Singh, GeetaAgnihotri [3], are discussed about Deep drawing process has been an important manufacturing process to produce automotive parts of good strength and light weight. There are many process parameters and other factors that affect product quality produced by deep drawing. Deep-drawing operations are performed to produce a light weight, high strength, low density, and corrosion resistible product. These requirements will increase tendency of wrinkling and other failure defects in the product.

P.VenkateshwarReddy,PerumallaJanakiRamulu,G.SandhyaMadhuri,DasariGovardhan and PVS Ram Prasad[4], are discussed about Deep drawing process is a significant metal forming process used in the sheet metal forming operations. Deep drawing process has different effectible process parameters from which an optimum level of parameters can be identified so that an efficient final product with required mechanical properties will be obtained. Punch forces and dome heights are evaluated for all the conditions.

#### i. Methodology

- . Static analysis is done for die and punch to determine the deformation.
- Modal analysis is done for die to determine the deformation and frequency for different materials by changing the geometry thicknesses.
- Random vibration analysis is done for die to determine the directional deformation.
- Transient analysis is done for die to determine the deformation

#### III. MODELING AND STATIC ANALYSIS OF DIE AND PUNCH

The time saved by using PTC CREO isn't the only advantage. It has many ways of saving costs. For instance, the cost of creating a new product can be lowered because the development process is shortened due to the automation of the generation of associative manufacturing and service deliverables. PTC also offers comprehensive training on how



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to use the software. This can save businesses by eliminating the need to hire new employees. Their training program is available online and in person, but materials are available to access anytime. A unique feature is that the software is available in 10 languages. PTC knows they have people from all over the world using their software, so they offer it in multiple languages so nearly anyone who wants to use it is able to do so

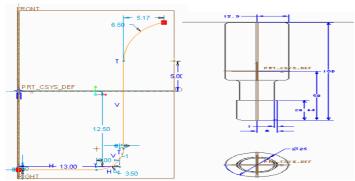


FIG1.1: 2D Sketch of DieFIG1.2:2D Sketch of Punch

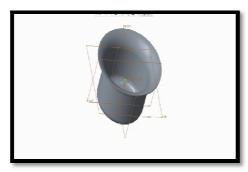


FIG1.3: 3D Model of Die



FIG1.4:3D Model of Punch

#### 1.1THEORETICAL CALCULATIONS TO FIND THE STRESS OF DIE

$$F = (\frac{2}{\sqrt{3}}) \times \pi \times UTS \times D \times t \qquad \dots (Eq 3.1)$$

Where,

t = thickness (mm)

UTS = Ultimate tensile strength (MPa)

Do = Die diameter (mm) = 26 mm

Blank diameter (D) = D =  $\sqrt{d2}$  - 4dh

 $D = \sqrt{25^2 - 4(25)} (25.0484)$ 

D = 24.4930 mm

Punch diameter = 25 mm

Blank thickness = 0.5, 0.7, 0.9 mm

Radial clearance between punch and die radius = 1.1mm

Punch nose radius = 0.52 mm



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Parameters obtained from Sandeeppatil [29]

 $\sigma = F/A$ 

---- (Eq3.2)

 $A = 333.923 \text{ mm}^2$ 

Where,

 $\sigma = \text{stress (N/mm}^2)$ 

P = maximum load (N)

 $A = Area (mm^2)$ 

#### **CASE 1- MATERIAL - STAINLESS STEEL**

At t = 0.5 mm,  $D_0 = 26 \text{ mm}$ 

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 513.61 \times 26 \times 0.5/333.923$$

= 62.5 MPa

At t = 0.7 mm,  $D_0 = 26 \text{ mm}$ 

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 513.61 \times 26 \times 0.7/333.923$$

= 54.4 MPa

At t = 0.9 mm,  $D_0 = 26 \text{ mm}$ 

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 513.61 \times 26 \times 0.9/333.923$$

= 40.5 MPa

#### CASE 2- MATERIAL - AL 5083

At t = 0.5 mm,  $D_0 = 26 \text{ mm}$ 

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 26 \times 0.5/333.923$$

= 46 MPa

At t = 0.7 mm,  $D_o = 26 \text{ mm}$ 

$$=\left(\frac{2}{\sqrt{2}}\right) \times \pi \times 228 \times 26 \times 0.7/333.923$$

= 45.07 MPa

At  $t = 0.9 \text{ mm}, D_0 = 26 \text{ mm}$ 



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$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 26 \times 0.9/333.923$$

= 32.199 MPa

#### CASE 3 - MATERIAL - AL 7475

At t = 0.5 mm,  $D_0 = 26 \text{ mm}$ 

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 345 \times 26 \times 0.5/333.923$$

= 63.2 MPa

At t = 0.7 mm,  $D_0 = 26 \text{ mm}$ 

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 26 \times 0.7/333.923$$

= 62 MPa

At t = 0.9 mm,  $D_0 = 26 \text{ mm}$ 

$$=\left(\frac{2}{\sqrt{2}}\right) \times \pi \times 228 \times 26 \times 0.9/333.923$$

= 48.7 MPa

Material Properties of Stainless Steel, AL5083, and AL7475

TABLE1.1:Material Properties of Stainless Steel, AL5083, and AL7475

Materials	Modulus Elasticity	Density	Tensile Yield	Ultimate Tensile	Poisson's Ratio
			Strength	Strength	
Stainless	77 - 310	0.19 -	25 –	34.5 -	0.22 -
Steel	GPa	9.01g/cc	2500	3100	0.346
			MPa	MPa	
AL 5083	71 GPa	2.66	228 MPa	317 MPa	0.22 -
		g/cc			0.33
AL 7475	70.3 GPa	2.81g/cc	462 MPa	531MPa	0.33

#### 2. STATIC ANALYSIS OF DIE

Static structural analysis for deformation and stress are shown in Figures respectively.

According to the contours plot, the maximum stress at inside of the die because of force acting on the area due to punch applied and the minimum stress at upside, According to the contours plot, the maximum stress at inside of the cup because of force acting on the area due to punch applied and the minimum stress at down side and around the die because of fixed the die.

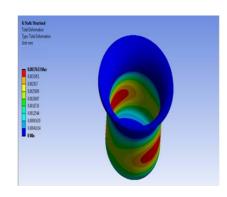


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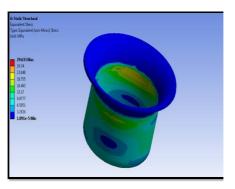


FIG2.1: Deformation Contours of D

FIG2.2: Stress Contours of Die

#### 2.1. THEORETICAL CALCULATIONS TO FIND THE STRESS OF PUNCH

$$F = \left(\frac{2}{\sqrt{3}}\right) \times \pi \times UTS \times D \times t$$

$$\sigma = F/A$$
, A=333.923 mm<sup>2</sup>

Stainless Steel

At t = 0.5 mm, Dp = 25 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 513.61 \times 25 \times 0.5/333.923$$

= 59.74 MPa

At t = 0.7 mm, Dp = 25 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 513.61 \times 25 \times 0.7/333.923$$

= 48.6 MPa

At t = 0.9 mm, DP = 25 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 513.61 \times 25 \times 0.9/333.923$$

= 42.54 MPa

AL 5083

At t = 0.5 mm, Dp = 25 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 25 \times 0.5/333.923$$

= 45.23 MPa



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At t = 0.7 mm, Dp = 25 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 25 \times 0.7/333.923$$

= 42.4 MPa

At t = 0.9 mm, Dp = 25 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 25 \times 0.9/333.923$$

= 41.11 MPa

AL 7475

At t = 0.5 mm, Dp = 25 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 345 \times 25 \times 0.5/333.923$$

= 55.23 MPa

At t = 0.7 mm, Dp = 25 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 25 \times 0.7/333.923$$

= 52.5 MPa

At t = 0.9 mm,  $D_p = 25 \text{ mm}$ 

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 25 \times 0.9/333.923$$

= 46.84 MPa

#### 3. STATIC ANALYSIS OF PUNCH

Static structural analysis of punch for deformation and stress are shown in Figures respectively.

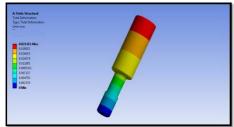


FIG3.1. Deformation contours OD punch

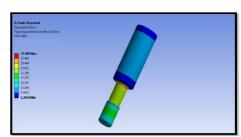


FIG3.2.Stress contours of Punch



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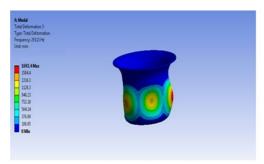
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#### IV. MODAL ANALYSIS OF DIE

The goal of modal analysis in structural mechanics is to determine the natural mode shapes and frequencies of an object or structure during free vibration. It is common to use the finite element method (FEM) to perform this analysis because, like other calculations using the FEM, the object being analyzed can have arbitrary shape and the results of the calculations are acceptable. The types of equations which arise from modal analysis are those seen in Eigen systems



**Fig4.1.Total Deformation contours** 

TABLE4.1 Modal analysis results of Die

Geometry (thickness) mm	Material	Mode shapes	Deformation(mm)	Frequency (Hz)
	Stainless steel	1	984.7	27046
		2	959.21	27165
		3	1019.4	28682
0.5	AL 7475	1	1649.1	27522
		2	1609	29463
		3	1692.4	29113
	AL 5083	1	1077.5	16819
		2	1050.1	16893
		3	1101.1	17767
	Stainless steel	1	792.16	30293
		2	845.6	36340
		3	803.61	30512
0.7	AL 7475	1	1293.5	30763
		2	1366.4	30812



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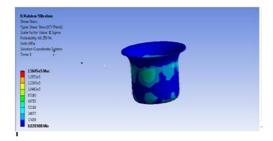
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		3	1315	31061
	AL 5083	1	838.27	18778
		2	881.18	18809
		3	851.19	18985
	Stainless steel	1	732.96	38113
		2	763.52	38341
		3	681.83	39293
0.9	AL 7475	1	1243.5	39798
		2	1282.4	39201
		3	1149.4	39594
	AL 5083	1	818.6	23717
		2	841.18	23853
		3	756.53	24531

### V. RANDOM VIBRATIONAL ANALYSIS OF DIE

The Random Vibration analysis uses the results from a modal analysis, specify which design scenario in the current model has the modal results with the Use modal results from Design Scenario field. The Model Units of the random vibration analysis must be

Identical to the Model Units of the modal results



#### FIG5.1.Shear Stress contour

Here, Table. shown Shear stress of AL5083, AL7475 and stainless steel, it can be seen that the minimum shear stress  $1.5e^5$  N/mm<sup>2</sup> for AL5083 and corresponding shear stress in AL7475 and Stainless steel are  $2.94e^5$  N/mm<sup>2</sup>,  $2,5.405e^5$  N/mm<sup>2</sup>.

The Shear stress value occurred minimum for the material AL 5083 at 0.9 mm thickness

#### 5.1. THEORETICAL CALCULATIONS FOR SHEAR STRESS

 $\tau = \text{Shear stress (N/m}^2)$ 



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---- (Eq 5.1)

u = Negligible  
Stainless Steel ---
$$\mu$$
 = 0.3  
At t = 0.5 mm, h = 25.0484 mm  
 $\tau$  = 4 × 0.3/(25.0484 - 0.5)  
= 49.8 N/m<sup>2</sup>  
At t = 0.7 mm, h = 25.0484 mm  
 $\tau$  = 4 × 0.3/(25.0484 - 0.7)  
= 49.6 N/m<sup>2</sup>  
At t = 0.9 mm, h = 25.0484 mm  
 $\tau$  = 4 × 0.3/(25.0484 - 0.9)  
= 48.8 N/m<sup>2</sup>  
AL 5083 --- $\mu$  = 0.129  
At t = 0.5 mm, h = 25.0484 mm  
 $\tau$  = 4 × 0.129/(25.0484 - 0.5)  
= 21.3 N/m<sup>2</sup>  
At t = 0.7 mm, h = 25.0484 mm  
 $\tau$  = 4 × 0.129/(25.0484 - 0.7)  
= 21.1 N/m<sup>2</sup>  
At t = 0.9 mm, h = 25.0484 mm  
 $\tau$  = 4 × 0.129/(25.0484 - 0.7)  
= 21 N/m<sup>2</sup>  
AL 7475 --- $\mu$  = 0.257

 $\tau = 4\mu u/(h-t),$ 

 $= 42.2 \text{ N/m}^2$ 

At t = 0.5 mm, h=25.0484 mm

 $\tau = 4 \times 0.257/(25.0484 - 0.5)$ 



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At t = 0.7 mm, h=25.0484 mm

 $\tau = 4 \times 0.257/(25.0484 - 0.7)$ 

 $= 42 \text{ N/m}^2$ 

At t = 0.9 mm, h = 25.0484 mm

 $\tau = 4 \times 0.257/(25.0484 - 0.9)$ 

Materials Thickness Analytical Theoretical

 $=41.8 \text{ N/m}^2$ 

TABLE5.2.Comparison of Theoretical and TABLE5.1.Random Vibration Analysis Results
Analytical Shear Stress Value

Geom

Mate

Directi

Shear

Shear

rviaceriais	(mm)	shear stress (MPa)	shear stress (MPa)	etry (thick ness)	rial	onal Deform ation	Stress (N/mm <sup>2</sup> )	Strain
Stainless steel	0.5	5.405×e5	4.9800×e5	(mm)		(mm)		
	0.7	2.945×e5	4.9600×e5		Stain less	128.1	5.405e5	7.3382
	0.9	1.5×e5	4.8800×e5		steel			
AL 5083	0.5	6.04×e5	2.1300×e5	0.5	AL 7475	191.79	2.945e5	11.046
	0.7	4.28×e5	2.1100×e5		AL 5083	116.86	2.642e5	6.7842
	0.9	1.651×e5	2.1000×e5		Stain	129.69	6.04e5	8.2066
AL 7475	0.5	9.77×e5	4.2340×e5		less steel	12,10,	010 100	0.2000
	0.7	4.72×e5	4.2200×e5	0.7	AL	249.98	4.28e5	15.899
	0.9	2.642×e5	4.1800×e5		7475			
					AL 5083	113.21	1.651e5	7.1378
					Stain less steel	2111.8	9.77e5	132.73
				0.9	AL 7475	2831.2	4.72e5	177.8
					AL 5083	1819	1.5e5	113.45



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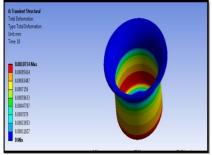
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### VI. TRANSIENT ANALYSIS OF DIE

A transient dynamic analysis is used to determine the response of a structure subjected to a time-dependent loading considering inertia and damping effects. It is often referred to as a time-history analysis. The full method in ANSYS uses the full system matrices to calculate the transient response at each solution point. The model-superposition method scales the mode shapes and sums them to capture the dynamic response.



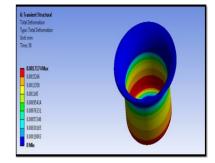


FIG 6.1 Deformation of cup at 10 second

FIG6.2.Deformation of cup at 20seconds

FIG6.3: Deformation of cup at 30sec

Below Figure from shows the maximum stress evaluated in leaf spring at 10, 20 and 30 sec for a given load.

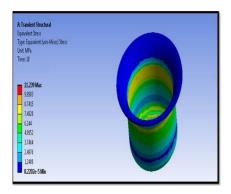


FIG6.4: Maximum stress of die at 10 seconds.

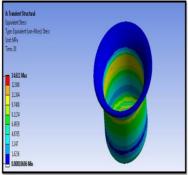


FIG6.5: Maximum stress of die at 20 seconds

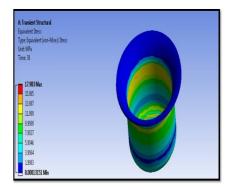


FIG6.6: Maximum stress of die at 30 seconds



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**TABLE6.1: Transient Analysis of Stainless Steel** 

Geometry	Time (sec)	Deformation	Stress	Strain
(thickness)		(mm)	(N/mm2)	
mm				
	10	0.00310	25.2051	3.902e-04
0.5	20	0.0051328	31.5041	4.5056e-04
	30	0.004521	39.0025	5.562e-04
	10	1.63e-03	21.2023	2.8700e-04
0.7	20	2.216e-03	27.403	3.5332e-04
	30	2.82e-03	31.011	3.9053e-04
	10	2.0107e-03	17.236	2.830e-04
0.9	20	1.904e-03	19.330	3.0310e-04
	30	2.130e-03	22.3014	3.0338e-04

**TABLE6.2: Transient Analysis of AL 7475** 

Geometry	Time (sec)	Deformation	Stress	Strain
(thickness)		(mm)	(N/mm2)	
Mm				
	10	0.0024670	21.302	3.53e-04
0.5	20	0.0030458	27.9653	4.1072e-04
	30	0.003760	35.064	5.0015e-04
	10	1.48e-03	18.1672	2.6710e-04
0.7	20	1.906e-03	22.673	3.03512e-04
	30	2.64e-03	27.601	3.7532e-04
	10	1.1205e-03	14.310	2.552e-04
0.9	20	1.420e-03	16.521	2.7348e-04
	30	1.821e-03	19.6520	2.9238e-04

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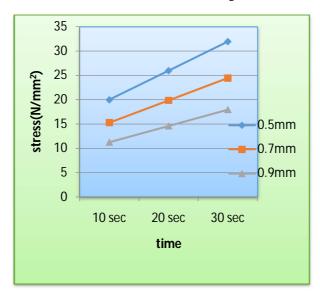
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**TABLE6.3: Transient Analysis of AL 5083** 

Geometry	Time (sec)	Deformation	Stress	Strain
(thickness)		(mm)	(N/mm <sup>2</sup> )	
mm				
	10	0.0021597	19.973	2.94e-004
0.5	20	0.0028076	25.965	3.8274e-04
	30	0.003454	31.957	4.7115e-04
	10	1.44e-03	15.287	2.1808e-04
0.7	20	1.876e-03	19.874	2.8352e-04
	30	2.30e-03	24.461	3.4896e-04
	10	1.0734e-03	11.239	1.649e-04
0.9	20	1.39e-03	14.611	2.1439e-04
	30	1.7174e-03	17.983	2.6357e-04

According to plot the accrues in stainless steel material of 0.9 mm, minimum at 0.9 mm Material AL-5083, Here Material thickness decreases, Shear Stress Will increases as shown in Fig



**GRAF6.1: Time Vs Stress** 



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#### VII. CONCLUSIONS

- From the static analysis of die & Punch it is seen that the stress values are increases by increasing the load and decreases with increasing the thickness and deformation values are increases by decreasing the loads at geometry thickness 0.9 mm for AL 5083 material when compared to stainless steel and AL7475.
- From the static analysis of cup AL5083 material having minimum stress value compared to AL7475 and stainless steel
- The static analysis of punch the stress values are increases by increasing load and deformation values are increases by decreasing the loads at geometry thickness 0.9 mm for AL 5083 material when compared to stainless steel and AL 7475
- From the static analysis punch AL5083 material having minimum stress value compared to AL7475 and stainless steel.
- The stress values are calculated using analytically as well as using theoretically for die and punch.
- The modal analysis of the die deformation values are increases by the loads. The deformation also increases mode shapes of the die. The maximum deformation of geometry thickness 0.5 mm for AL 7475.
- The random vibration analysis the shear stress value are increases by increasing the geometry thickness at 0.9 mm in AL5083.
- The shear stress values are calculated using analytically as well as theoretically for die.
- The transient analysis of die the stress values are increases by increasing load and deformation values are increases by decreasing the time at geometry thickness 0.9 mm for AL 5083 material when compared to stainless steel and AL 7475.
- So it can be concluded the geometry thickness is 0.9 mm and material is AL 5083 is best for die and punch.

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